

Whistling Pines Drainage Calculations:

Inlet Between Lots 14 & 15 (SS Sta. 0+00, Inlet No. 1):

Runoff, $Q_{100} = 64.6$ cfs (off-site flow from detention calculations)

Inlet control available head, HW = 3 ft. (inv. = 435, ground = 438)

30" pipe HW/D = 1.2

From attached nomograph 30" Q = 40 cfs

Use double 30", capacity = 80 cfs

Inlets at Sta. 5+75 (SS Sta. 1+50, Inlet No. 2):

Area North of Lot 15 & West of Lot 19:

Drainage area, A = 1.2 acres

Runoff Coefficient, $C_{100} = 0.70$

Length of overland flow = 120 feet, Slope of overland flow = 2%

Length of gutter channelized flow = 280 feet, Slope of channelized flow = 3.9%

From attached nomographs with overland flow roughness coefficient = 0.40, channelized flow roughness coefficient = 0.02, $t_c = 14.2$ minutes

$i = 8.0$ in/hr (100 year flood)

Flow From Inlet at SS Sta. 0+00:

Length of overland flow = 150 feet, Slope of overland flow = 3%, $n = 0.40$, $t_c = 13.1$ min.

Length of shallow conc. flow = 675 feet, Slope of, shallow conc. flow = 3%, $n = 0.03$, $t_c = 7.3$ min.

Length of natural channel flow = 850 feet, Slope of channel = 2%, $n = 0.03$, $t_c = 12.2$ min.

Length of pipe flow = 125 feet, Slope of pipe flow = 0.8%, $n = 0.012$, $t_c = 0.3$ min.

Total $T_c = 32.9$ min.

$i = 5.4$ in/hr (100 year flood)

$Q_{100} = 67.5$ cfs (from computation sheet)

Inlets at Sta. 7+00 (SS Sta. 2+70, Inlet No. 3):

Area North of Lot 29 & West of Lot 21:

Drainage area, A = 1.3 acres

Runoff Coefficient, $C_{100} = 0.70$

Area of Lot 14 & north half of Lot 13:

Drainage area, A = 0.3 acres

Runoff Coefficient, $C_{100} = 0.70$

From attached nomographs with overland flow roughness coefficient = 0.40, gutter flow roughness coefficient = 0.02, $t_c = 13.7$ minutes

$i = 8.1$ in/hr (100 year flood)

Flow From Inlet at SS Sta. 1+25 to 2+55:

Length of overland flow = 150 feet, Slope of overland flow = 3%, $n = 0.40$, $t_c = 13.1$ min.
Length of shallow conc. flow = 675 feet, Slope of, shallow conc. flow = 3%, $n = 0.03$, $t_c = 7.3$ min.
Length of natural channel flow = 850 feet, Slope of channel = 2%, $n = 0.03$, $t_c = 12.2$ min.
Length of pipe flow = 125 feet, Slope of pipe flow = 1.0%, $n = 0.012$, $t_c = 0.3$ min.
Length of pipe flow = 130 feet, Slope of pipe flow = 1.20%, $n = 0.012$, $t_c = 0.3$ min.
Total $T_c = 33.2$ min.
 $i = 5.3$ in/hr (100 year flood)

$Q_{100} = 72.1$ cfs (from computation sheet)

Inlets at Sta. 9+25 (SS Sta. 5+20, Inlet No. 4):

Area south of street west of Sta. 7+00 & south half of Lot 13:

Drainage area, $A = 0.7$ acres
Runoff Coefficient, $C_{100} = 0.70$

Area North of street & southwest half of Lot 28:

Drainage area, $A = 0.4$ acres
Runoff Coefficient, $C_{100} = 0.70$

Area west of street & east of Lot 20:

Drainage area, $A = 1.8$ acres
Runoff Coefficient, $C_{100} = 0.70$

From attached nomographs with overland flow roughness coefficient = 0.40, gutter flow roughness coefficient = 0.02, $t_c = 15.1$ minutes

$i = 7.7$ in/hr (100 year flood)

Flow From Inlet at SS Sta. 2+55 to 5+20:

Length of overland flow = 150 feet, Slope of overland flow = 3%, $n = 0.40$, $t_c = 13.1$ min.
Length of shallow conc. flow = 675 feet, Slope of, shallow conc. flow = 3%, $n = 0.03$, $t_c = 7.3$ min.
Length of natural channel flow = 850 feet, Slope of channel = 2%, $n = 0.03$, $t_c = 12.2$ min.
Length of pipe flow = 125 feet, Slope of pipe flow = 0.8%, $n = 0.012$, $t_c = 0.3$ min.
Length of pipe flow = 395 feet, Slope of pipe flow = 2.0%, $n = 0.012$, $t_c = 1.3$ min.
Total $T_c = 34.2$ min.
 $i = 5.2$ in/hr (100 year flood)

$Q_{100} = 81.1$ cfs (from computation sheet)

Proposed 18" at Sta. 9+25:

Drainage area, $A = 2.2$ acres
Runoff Coefficient, $C_{100} = 0.70$
Rainfall intensity, $i_{100} = 6.7$ in/hr (100 year flood)
Runoff, $Q_{100} = (0.70)(6.7)(2.2) = 10.3$ cfs

The proposed 18" drainage pipe (1.0% slope) has a capacity of 11.3 cfs.

Proposed 42" to Detention Pond:

$$Q_{100} = 81.1 \text{ cfs}$$

The proposed 42" drainage pipe (1.0% slope) has a capacity of 126.0 cfs.

The proposed 42" drainage pipe (1.0% slope) has a capacity of 126.0 cfs. The velocity of the pipe discharge at the maximum capacity rate is 13.1 fps, which is greater than 7 fps, therefore rock riprap erosion protection will be required at the pipe outlet.

Whistling Pines Gutter Capacity Calculations:

$$\text{Gutter Capacity, } Q = \frac{0.56}{n} S_x^{1.67} S^{0.5} T^{2.67}$$

$$n = 0.015$$

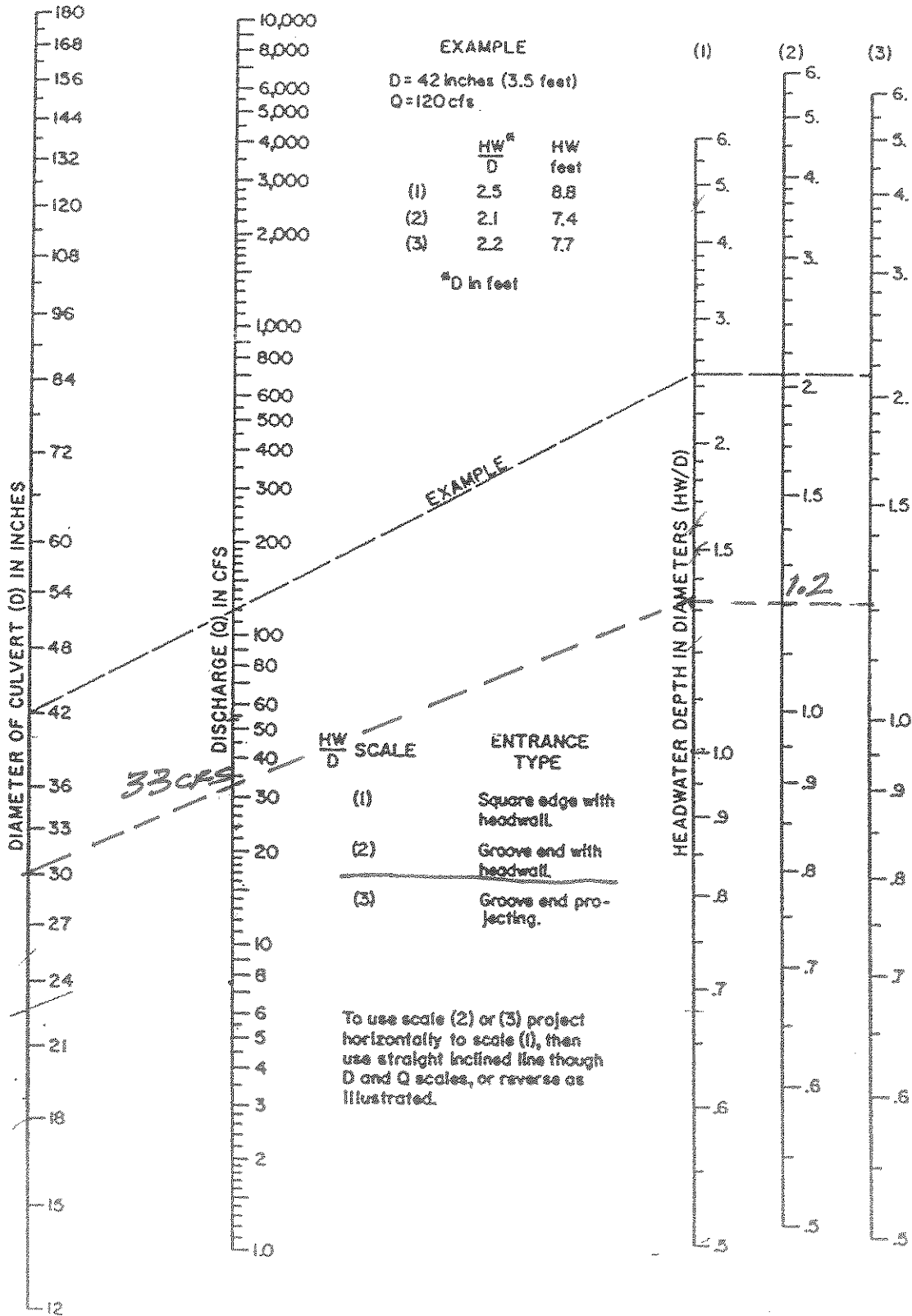
$$S_x = 0.33/13 = 0.025$$

$$T = 13'$$

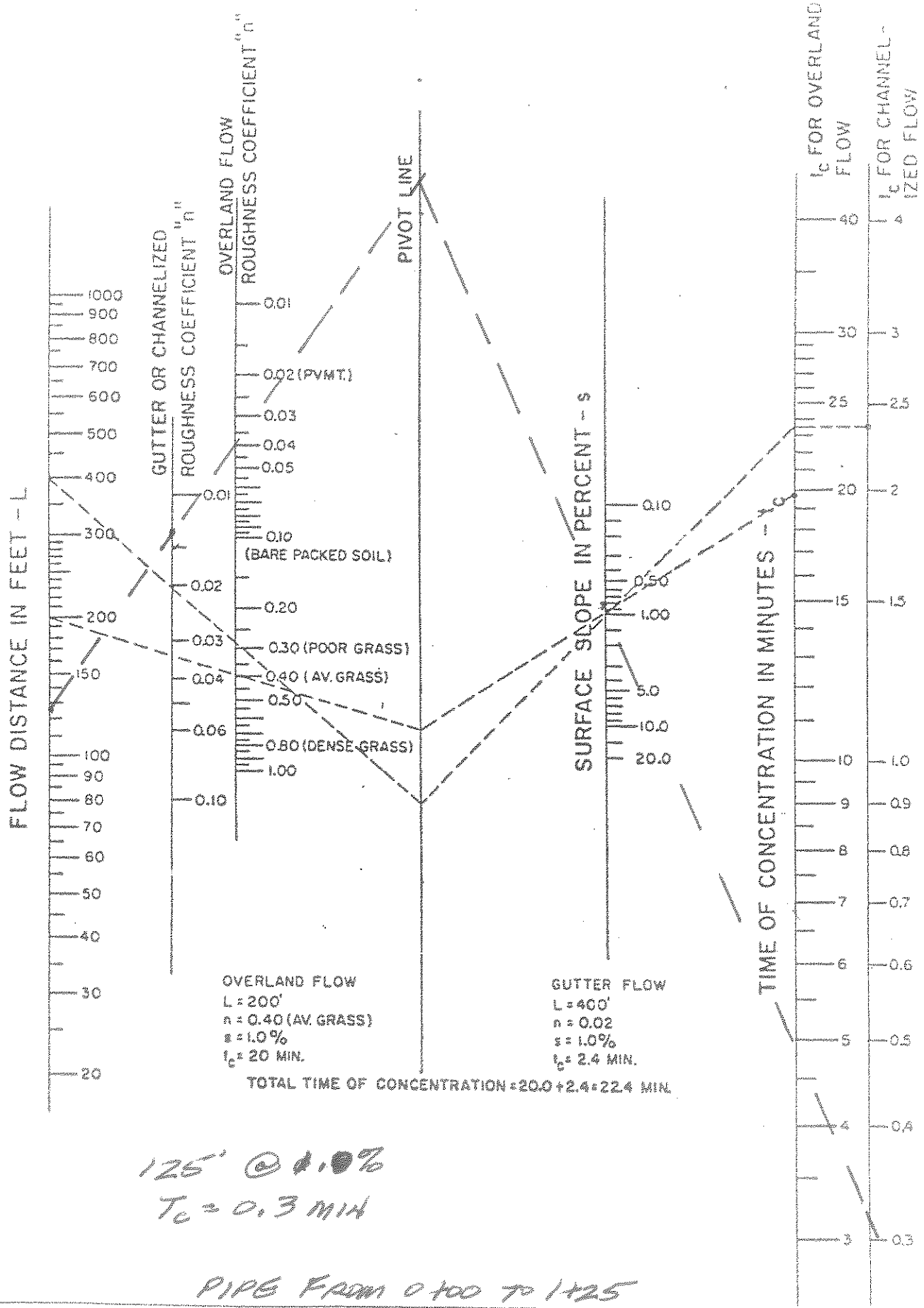
$$Q = 73.9 S^{0.5} \text{ (single gutter capacity)}$$

Street Section	Slope, %	Single Gutter Capacity, cfs	Maximum Flow In Section, cfs
0+00 to 1+48	2.23	11.0	3.3
3+00 to 1+48	2.04	10.6	1.5
3+00 to 5+90	3.92	14.6	8.3
5+90 to 7+00	0.52	5.3	2.3
7+00 to 9+25	0.52	5.3	3.6
12+73 to 9+25	4.79	16.2	10.7

PLOT F - HEADWATER DEPTH FOR CONCRETE PIPE CULVERTS WITH INLET CONTROL



INLET CULVERT AT LOT 14/15
 INLET No. 1



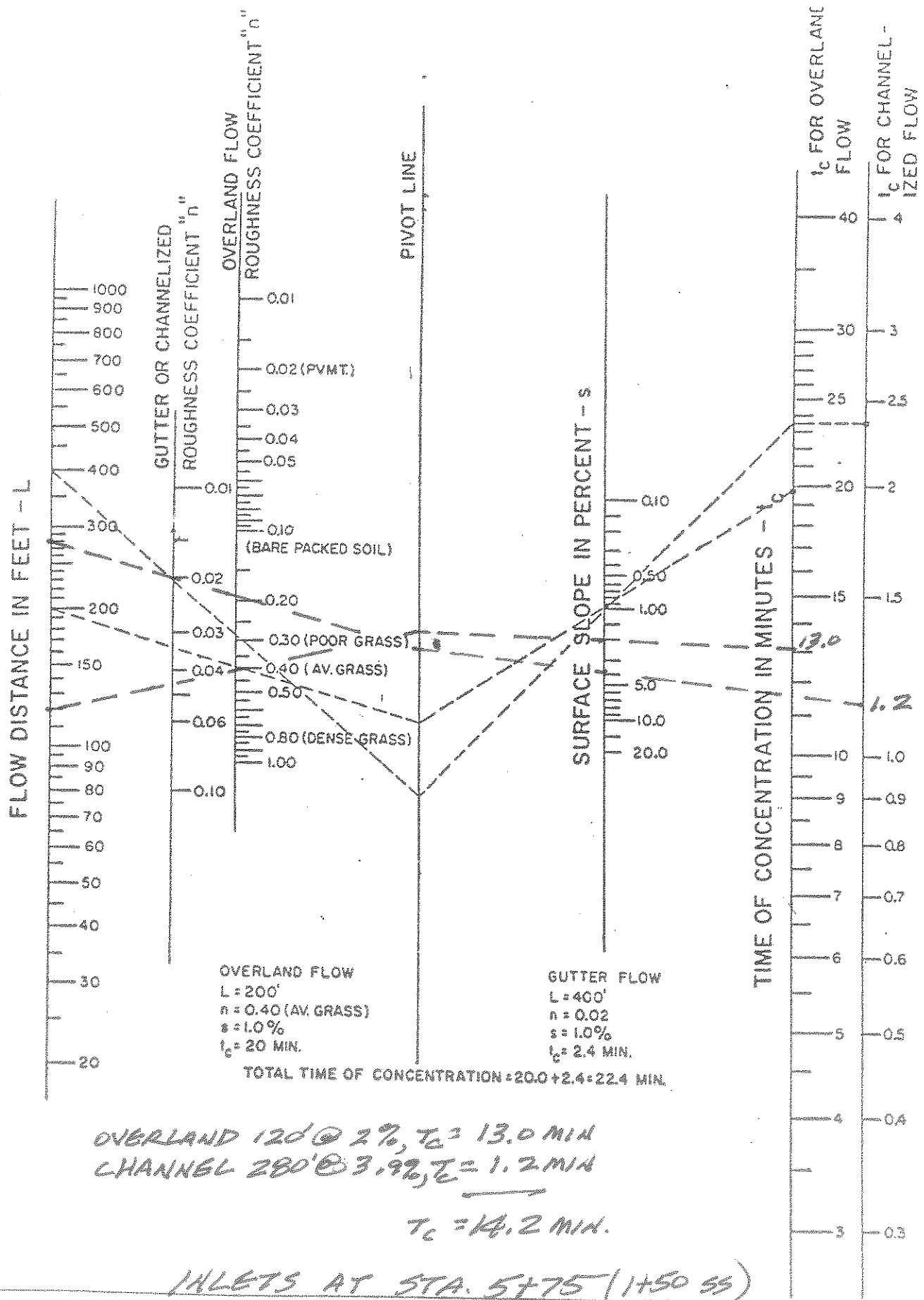
125' @ 1.0%
 $T_c = 0.3$ MIN

PIPE FROM 0+100 TO 1+25



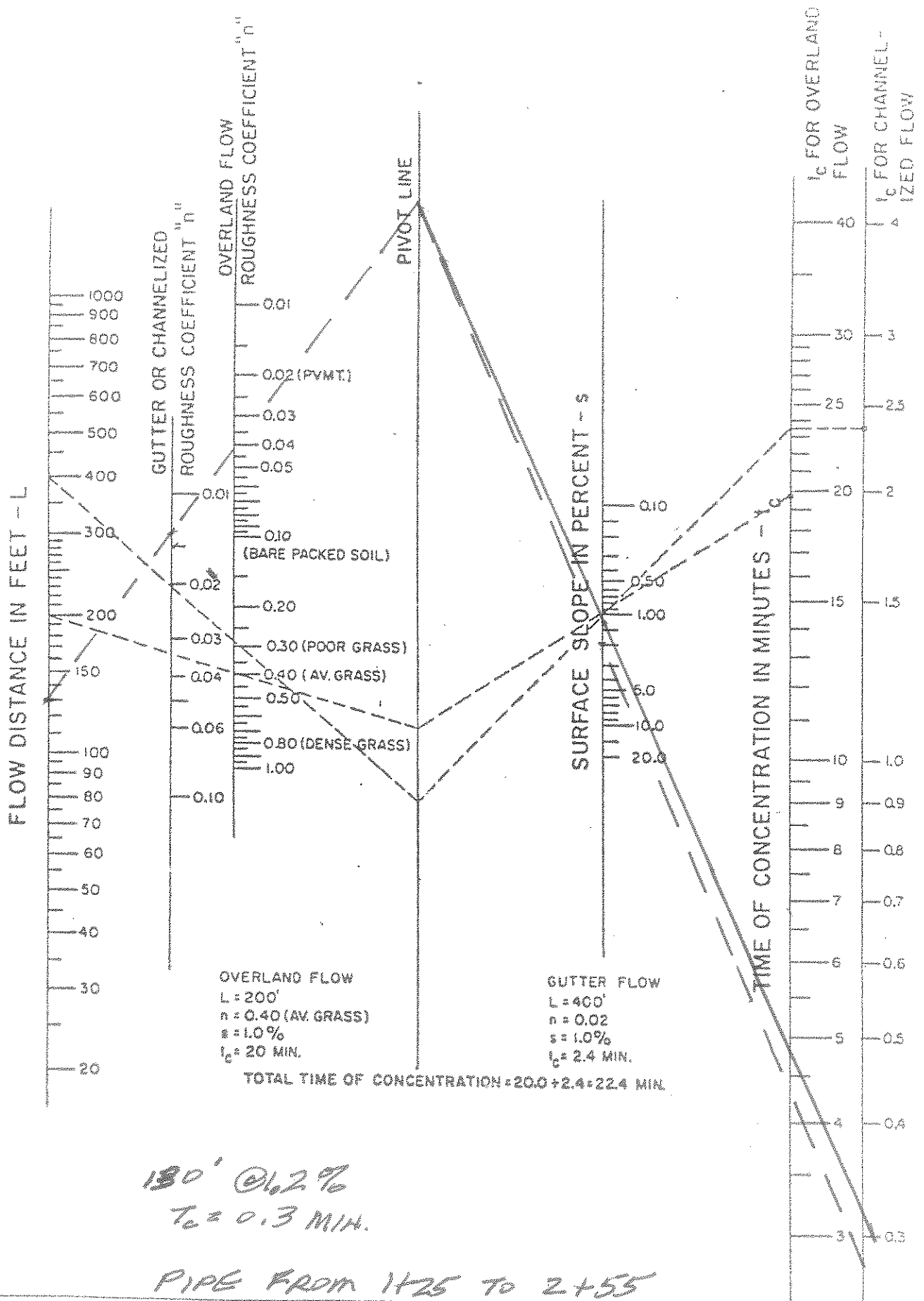
NOMOGRAPH FOR TIME OF CONCENTRATION

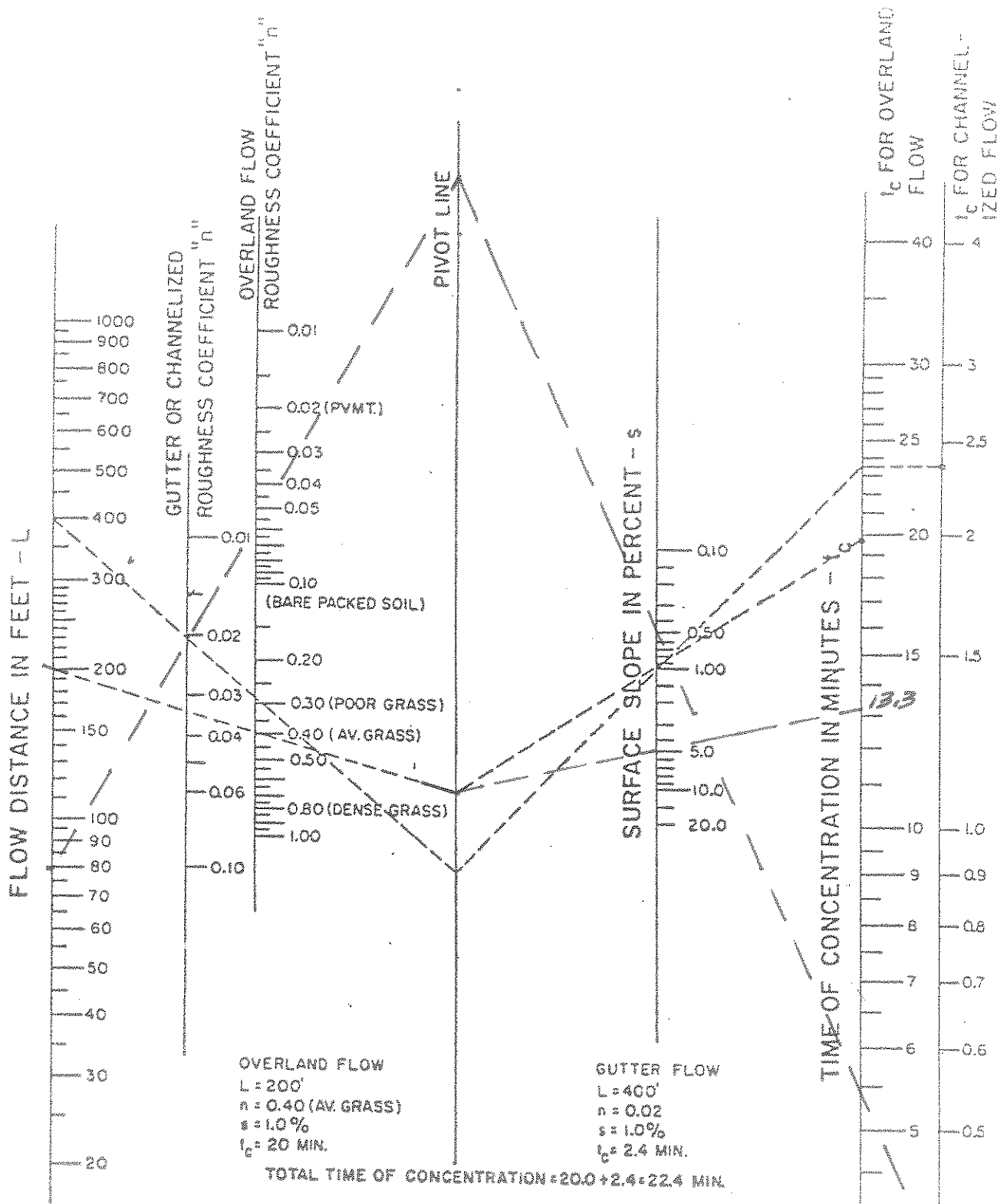
SOURCE: City of Fort Worth, Tx.



NOMOGRAPH FOR TIME OF CONCENTRATION

SOURCE: City of Fort Worth, Tx.





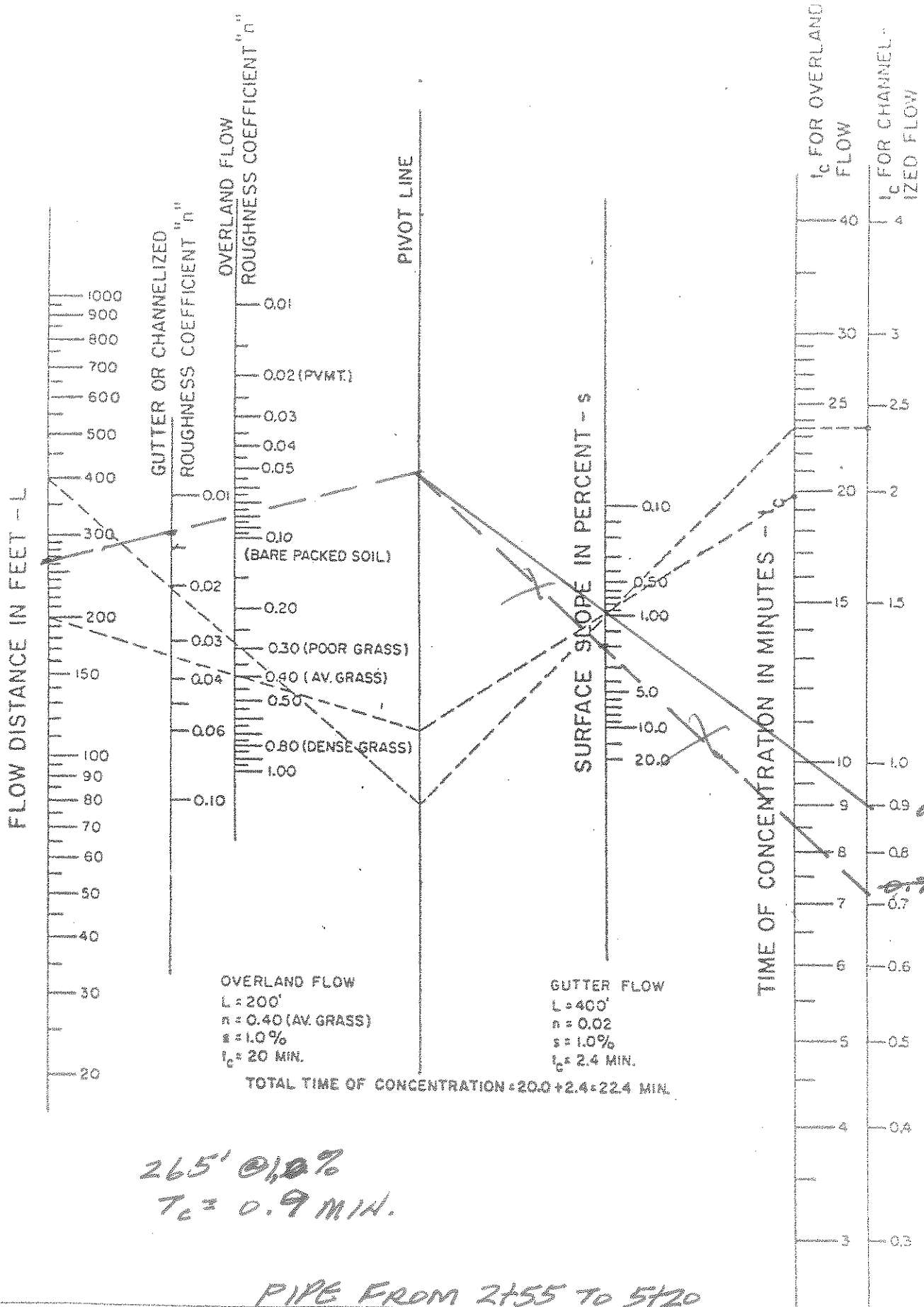
OVERLAND 200' @ 5%, $t_c = 13.3$
 GUTTER 80' @ 0.5%, $t_c = 0.4$
 $t_c = 13.7$

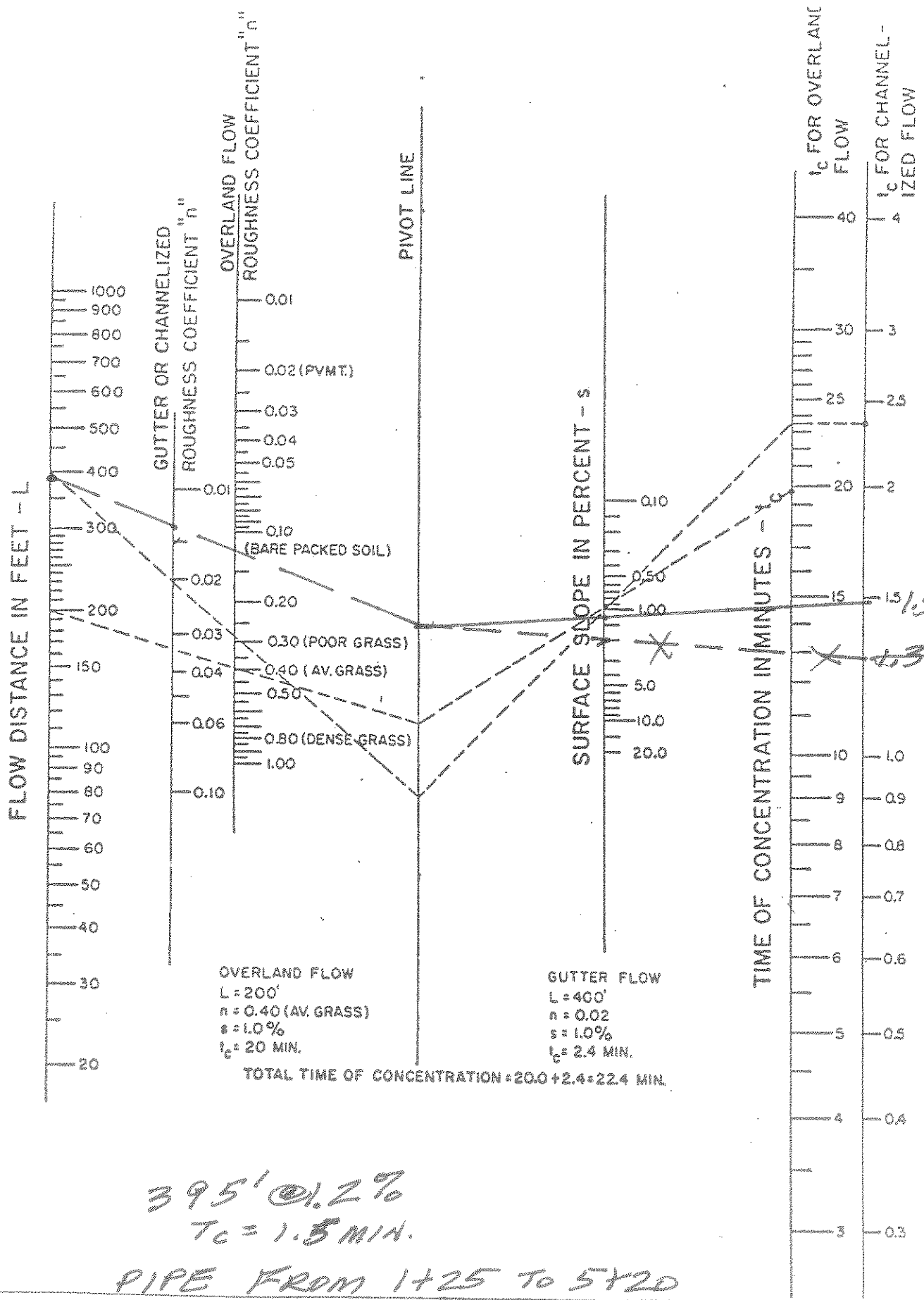
INLETS AT STA. 7+00 (SS 2+70)

INLET NO. 3
 NOMOGRAPH FOR TIME OF CONCENTRATION



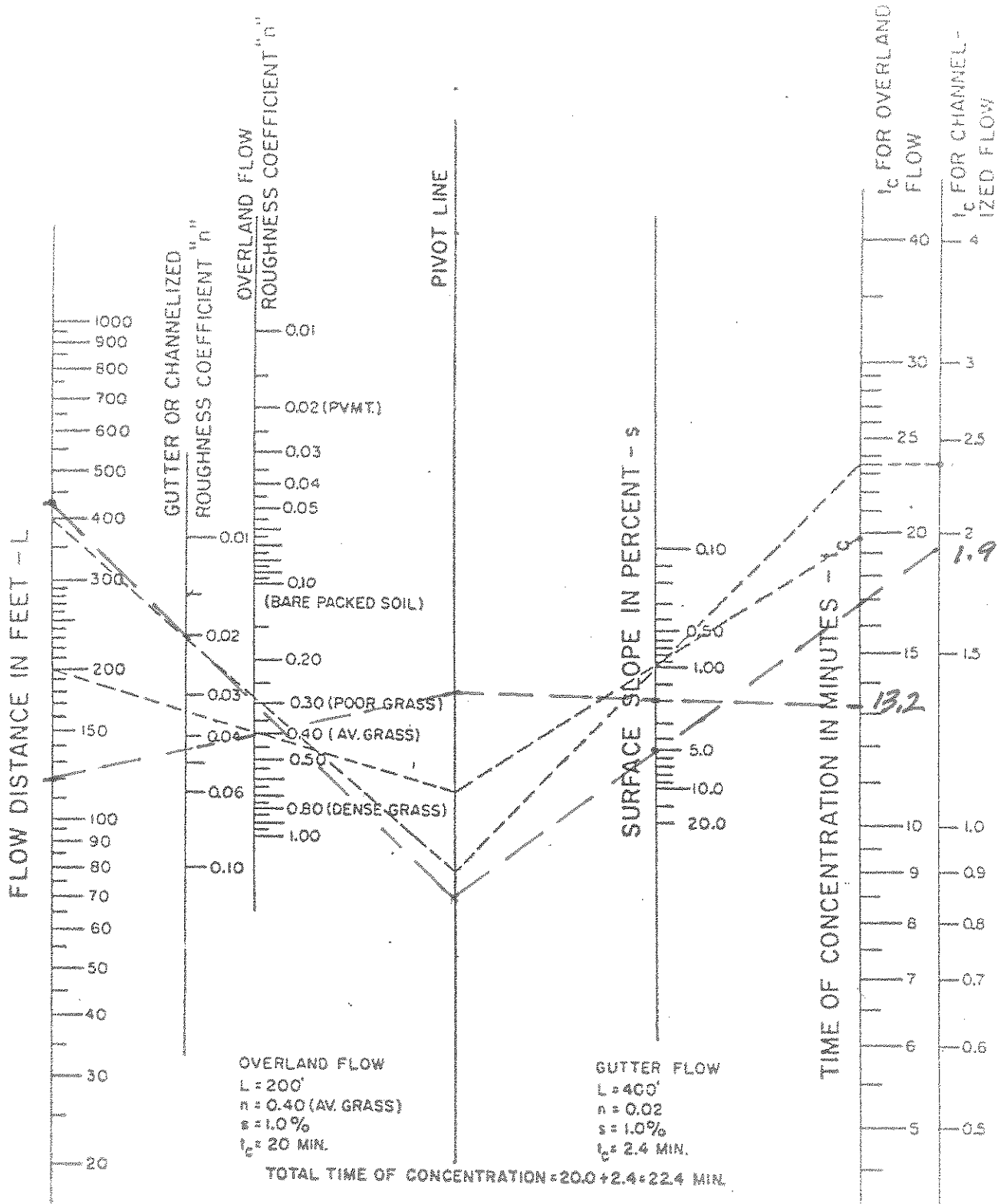
SOURCE: City of Fort Worth, Tx.





NOMOGRAPH FOR TIME OF CONCENTRATION

SOURCE: City of Fort Worth, Tx.



OVERLAND 120' @ 2%, $T_c = 13.2$ MIN.
 GUTTER 430' @ 5%, $T_c = 1.9$ MIN.

$T_c = 15.1$ MIN

INLETS AT STA. 9+25 (SS 5+20)

INLET No. 4

NOMOGRAPH FOR TIME OF CONCENTRATION



City of Little Rock

SOURCE: City of Fort Worth, Tx.

2-2

FIGURE

